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# GAS CHROMATOGRAPHY (GC)

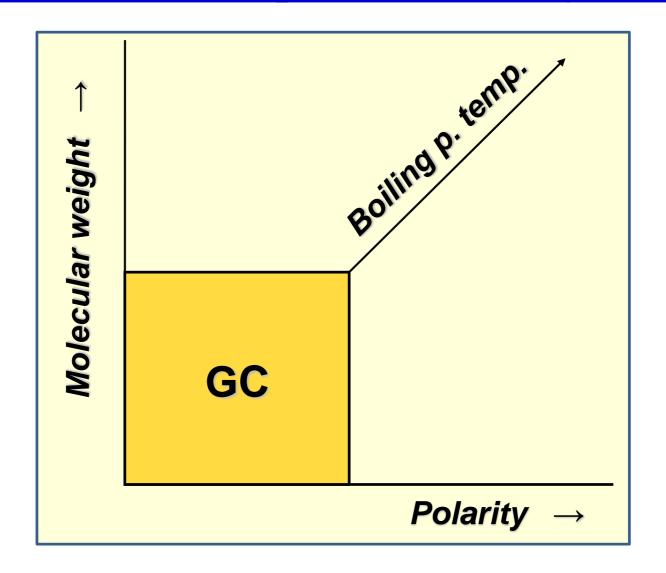
Partition between stationary and mobile phase

- based on differences in volatility and structure (separated compounds show the different chromatographic affinity)

### **Suitable for:**

- thermostable compounds and nonreactive with others
- inorganic compounds are mostly not GC amenable (applicable for  $H_2O$ , gases etc.)
- with acceptable volatility at 350 °C it must be at least partially in the gaseous state (possibility of derivatization)

# Estimation of compound suitability for GC



## TECHNICAL REALIZATION OF GC

## **Injection - injector**

Split/splitless, on-column, pulse techniques

Large volume injection (PTV, on-column-SVE)

Desorption techniques

# **Separation – column**

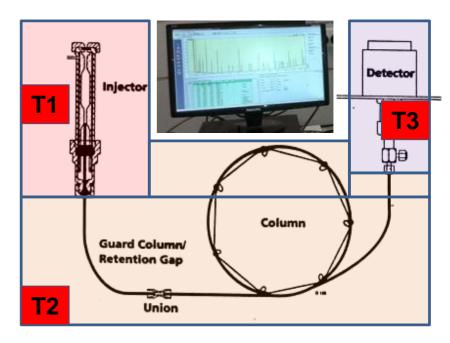
Packed and capillary columns
Parallel and multidimensional GC

### **Detection - detector**

Retention time, spectrum

## **Quantification - software**

Detector response - peak area or height



### **GC SEPARATION THEORY**

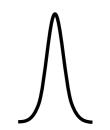
After introduction to column molecules are **partitioning** between stationary (SP) and mobile phase (MP), system is almost in equilibrium – distribution between SP and MP is possible to describe using distribution constant  $\mathbf{K}_{\mathbf{D}}$ 

All molecules are moving only in mobile phase, all molecules go through the same path at different times according to their different affinity to the stationary phase.

**Each molecule can enter stationary phase** – one enters, one exits, the distribution between phases is kept in repeating equilibrations for each molecule.

If the position is occupied, the molecule travels further until it finds a free space. Another molecule may enter the released site. With a large number of molecules oversaturation of column can appear. Typical consequences of the column oversaturation is either fronting or tailing of peaks, in the extreme case, a significant reduction of retention times.

#### **NORMAL**



**FRONTING** 



**TAILING** 



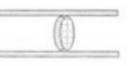
Separation of 2 compounds is achieved, if they have different distribution between stationary and mobile phase.

#### **IMPROVEMENT OF SEPARATION**

1. Increasing of differences in retention times

(thermodynamic aspect) – affecting of interactions between analyte and stationary phase

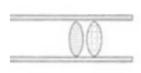
= changes of  $K_D$  and temperature





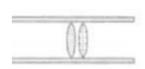
2. Narrowing of elution bands

(kinetic aspect) – column dimensions, film thickness of SP, mobile phase speed





narrow elution bands needs less separation than wide ones





### MAJOR FACTORS AFFECTING SEPARATION

**Stationary phase** – **higher solubility (affinity)** of analyte in SP ⇒ **higher retention** 

**Analyte structure** – differences in solubility of analytes in stationary phase

**Temperature** – affects distribution of molecules between SP and MP

 $\uparrow$  temperature  $\Rightarrow \uparrow$  number of molecules in MP

 $\Rightarrow \downarrow t_R$  and  $\downarrow$  separation)

⇒ narrower elution zones with lower retention times

Other factors: column dimensions, carrier gas and its velocity

## **Capacity factor (retention factor – k or k')**

#### It depends on: column SP and dimensions, temperature, MP linear velocity

Molecules of any analyte pass through the same length (volume) of column, which is the so-called dead (elution) volume expressed as the retention time of an analyte passing through the system without delay at time  $t_0$  (or  $t_M$ )

 $\Rightarrow$  reduced retention time  $t_R$ ' expressing the time spent in SP is obtained for a given analyte as the retention time  $t_R$  reduced by the dead retention time  $t_R$   $\Rightarrow$   $t_R$ ' =  $t_R$  -  $t_0$ , the retention times of the analytes thus differ by the difference in the times spent in the SP

#### ⇒ definition of capacity factor:

ratio of times spent by analyte in SP  $t_R$ , and in MP  $t_0$ 

$$k = t_R' / t_0 = (t_R - t_0) / t_0$$

A measure of retention of a compound in SP compared to another one

$$k = 0 \Rightarrow$$
 no retention,  $k \approx 1 \Rightarrow$  low retention,  $k \approx 10 \Rightarrow$  high retention

- characterization of GC separation in terms of speed

# Distribution constant (Partition coefficient or ratio - K<sub>D</sub>)

#### **Distribution constant definition**

- ratio of molar concentration of analyte in SP  $(c_S)$  and in MP  $(c_M)$
- expresses the distribution of analyte between SP and MP
- constant for the given analyte, SP and temperature

Analytes are partitioned between SP and MP depending on the column temperature, their structure and the nature of the SP (chromatographic affinity).

$$\mathbf{K_D} = \mathbf{c_S} / \mathbf{c_M} = \mathbf{k} \beta = (\mathbf{t_R}' / \mathbf{t_0}) (\mathbf{r} / \mathbf{2} \mathbf{d_f})$$
  
 $\beta = \mathbf{r} / 2 \mathbf{d_f} = \mathbf{V_M} / \mathbf{V_S}$  is phase ratio

## <u>Distribution constant – important relations</u>

$$\mathbf{K_D} = \mathbf{c_S} / \mathbf{c_M} = \mathbf{k} \ \beta = (\mathbf{t_R'} / \mathbf{t_0}) \ (\mathbf{r} / \mathbf{2} \ \mathbf{d_f}), \ \beta = \mathbf{r} / 2 \ \mathbf{d_f} = \mathbf{V_M} / \mathbf{V_S} \ \text{is phase ratio,}$$
  
$$\Rightarrow \mathbf{k} = \mathbf{K_D} / \beta = \mathbf{K_D} \mathbf{2} \ \mathbf{d_f} / \mathbf{r}$$

- useful for the estimation of the impact of changes in column parameters on column retention and efficiency during method optimization
- for  $\uparrow$  k is necessary  $\uparrow$  K<sub>D</sub> or  $\downarrow$   $\beta$  vice versa  $\uparrow$   $\beta \Rightarrow \downarrow$  k (at constant K<sub>D</sub>)

$$\beta = r/2 d_f \Rightarrow \uparrow \beta \approx \uparrow r$$
 i.e.  $\uparrow$  column radius or  $\approx \downarrow d_f$  i.e.  $\downarrow SP$  thickness

Relationship containing column length and MP (carrier gas type and flow rate)

$$\begin{aligned} t_R' &= t_0 \; (2 \; c_S \, d_f) \, / \, (c_M \, r) \; ; \; t_0 = L \, / \, u \\ \Rightarrow t_R' &= (2 \; c_S \, d_f \, L) \, / \, (c_M \, r \, u) = \quad (c_S \, / c_M) \qquad (2 \; d_f \, / r) \quad (L/u) \\ \hline K_D \qquad \qquad 1/\beta \qquad t_0 \end{aligned}$$

## <u>Distribution constant – practical aspects</u>

## Influence of temperature on K<sub>D</sub>

- $\uparrow$  temperature  $\Rightarrow \downarrow K_D \Rightarrow \downarrow$  retention
- small change in temperature = large change in retention (c.  $\beta$ )
- $\uparrow K_D \Rightarrow$  stronger connection with  $SP \Rightarrow \uparrow t_R$
- multiple mass transfer = longer analysis = more of analyte in SP, where it does not move  $\Rightarrow$  analyte is introduced into detector for a long time in the broaden zone  $\Rightarrow$  wide peak
- $\downarrow K_D \Rightarrow$  more of analyte in MP =  $\downarrow t_R$
- fast transfer to detector = narrow peak
- $\mathbf{K}_{\mathbf{D}}$  changes are not the same for all analytes suitable temperature programming is necessary
- at the beginning of the analysis  $\uparrow K_D$  (lower temperature) improves separation
- at the end of the analysis  $\downarrow K_D$  (higher temperature) = narrower peaks

## Separation factor or selectivity - α

### Ability of SP to separate 2 compounds

- retention ratio of the two peaks  $\approx$  the distance between the tops of two peaks
- no information about the quality of elution zone (peak shape)
- the same for wide (overlaid) or narrow peaks

$$\alpha = k_2 / k_1 = (t_{R2} - t_0) / (t_{R1} - t_0)$$

- determined by functional groups
  - $\approx$  depends on specific interactions of analytes with SP
- if > 1, compounds can be separated (sometimes only partially)
- $if \le 1$ , compounds cannot be separated in the given system

**Efficiency** ≈ performance

Expressed as a number of theoretical plates – n (N)

- $\uparrow$  efficiency  $\Rightarrow \downarrow$  width of the elution zone  $\Rightarrow \uparrow$  separation potential narrower elution zones = higher peak capacity
- dimensionless parameter calculated for 1 analyte, i.e. does not characterize the separation of 2 compounds
- relationship between retention time and peak width

$$n = 16 (t_R/w_b)^2 = 5,545 (t_R/w_h)^2$$

w<sub>b</sub> – peak width at the baseline, w<sub>h</sub> - peak width at half height

### Efficiency = number of theoretical plates - n (N)

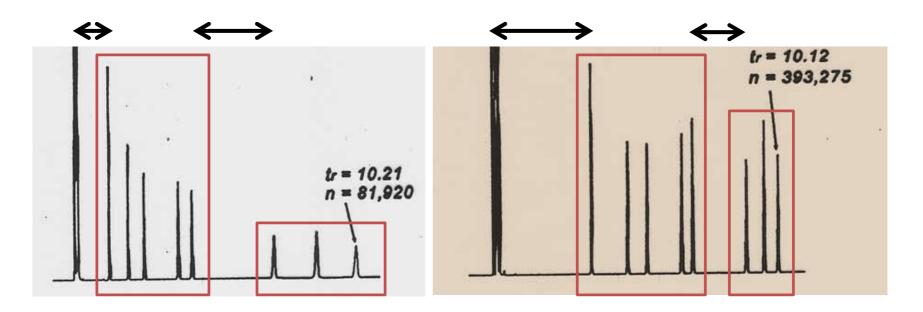
- n is given by the compound selection for the calculation, i.e. by retention time and shape of peak used for calculation!
- n is higher for earlier eluted compounds and with increasing of their retention times decrease (elution zones are widening)
- correct characterization of the column peak with k > 5 (linear dependence of n and k)
- column efficiency comparison peaks with identical k value
- calculated n actually describes the efficiency of the whole analytical system and method (injection, carrier gas, flow rate, column temperature etc.)
- narrowing of peaks by temperature programming fundamental influence on the n value

## Efficiency (number of theoretical plates) – temperature effect

 $\downarrow$  width of the elution zone  $\Leftrightarrow \uparrow$  efficiency

isothermal

vs. programmed temperature



Height equivalent to a theoretical plate (HETP) – h

$$\downarrow$$
 h  $\Rightarrow \uparrow$  n  $\Rightarrow \uparrow$  efficiency

One theoretical plate = part of the column, in which occurs once the equilibration

- number of theoretical plates - total or per meter of column length

$$n = L/h$$
 (HETP)

- change of the theoretical plates number in time  $\Rightarrow$  checking after a defined number of analyzes = officially acceptable evidence of changes of column properties e.g. for accredited analyzes
- ⇒ shortening vs. column replacement

## **Resolution - R**

The degree of separation between two peaks with respect to their width - a measure of the quality of the compounds separation

R is given by efficiency (n  $\approx$  peak shape), SP selectivity ( $\alpha$ ) and retention time (k)

$$\mathbf{R} = 1/4 \ \mathbf{n}^{1/2} ((\alpha - 1)/\alpha) \ (\mathbf{k}/(\mathbf{k} + 1))$$

$$R = 1,18 (t_{R2} - t_{R1}) / (w_{h1} + w_{h2})$$

R < 1.5 (partial) peak overlap; lower n and  $\alpha$ 



R = 1.5 peaks separated with zero spacing between them



R > 1.5 peaks separated with spacing between them; higher n and  $\alpha$ 

Effects on elution zones (peak shape) - broadening and other deformations

Theory developed for packed columns (subsequently simplified for capillary columns)

### 1. Eddy (turbulent) diffusion in MP ( $H_F$ ) $\approx$ A (m)

Flow between sorbent particles is different because of different distances between them (channels)  $\Rightarrow$  molecules of analytes move with different speed.

### 2. Molecular longitudinal diffusion in MP ( $H_L$ ) $\approx$ B ( $m^2$ s<sup>-1</sup>)

Analyte is concentrated at the column head in narrow zone  $\Rightarrow$  during elution occurs zone broadening by diffusion from higher concentration in zone centre to lower concentration at the edges of elution zone (Fick's law). Effect decreases with  $\uparrow \underline{u}$  [m s<sup>-1</sup>].

#### 3. Resistance to mass transfer in SP ( $H_S$ ) $\approx$ C (s)

Molecules diffuse between mobile and stationary phase, with different deep  $\Rightarrow$  different retention. Molecules in mobile phase are faster then ones in stationary phase  $\Rightarrow$  band broadening.

#### 4. Resistance to mass transfer in MP ( $H_M$ ) $\approx$ C (s)

Inconsistent mobile phase flow in capillary column (in channels between particles) – at wall (sorbent surface) is minimal X in the middle of stream maximal  $\Rightarrow$  molecules move with different speed. Diffusive transfer of molecules between streams – compensation of differences. Effect increases with  $\uparrow \underline{u}$  [m s<sup>-1</sup>].

$$H = H_F + H_L + H_S + H_M = A + B/u + (C_S + C_M) u$$
  
 $H = A + B/u + C u$ 

## Selection of parameters to achieve the required resolution

- 1. <u>Temperature programming, pressure programming, different column lengths and diameters, different SP thicknesses</u>
  - effect on peak width, retention time (elution order may change), peak capacity, peak distribution on the chromatogram
- 2. <u>Selection of stationary phase</u> difference in character and retention, difference in selectivity there is a change in the elution order, different effect on different analytes application of parallel chromatography on two different SP
- 3. <u>Selection of mobile phase</u> different carrier gases, differences in optimum flow rates

## Column dimensions - efficiency and resolution

$$R = 1/4 n^{1/2} ((\alpha-1)/\alpha) (k/(k+1))$$

$$t_R' = (2 c_S d_f L)/(c_M r u) = (c_S / c_M) (2 d_f / r) (L / u)$$
  
 $n = L / h;$   $n = 16 (t_R / w_b)^2$ 

**Length:**  $\uparrow L \Rightarrow \uparrow n$   $2x \uparrow L \Rightarrow \uparrow R$  but only about 25 - 35 %

Inner diameter:  $\downarrow r \Rightarrow \uparrow n$   $4x \downarrow r \Rightarrow 2x \uparrow R$ 

**SP film thickness:**  $\uparrow \mathbf{d_f} \Rightarrow \uparrow \mathbf{retention}$ 

<u>Highly volatile compounds (k < 5):</u>  $\uparrow d_f \Rightarrow \uparrow n$ 

Less volatile compounds (k > 5):  $\uparrow d_f \Rightarrow \downarrow n$  (elution at higher T

⇒ band broadening)

## Temperature - efficiency and resolution

### **↑ temperature** ⇒ ↓ retention

#### The effect on resolution is not unequivocal, but it is significant.

Temperature affects not only retention but also peak width, i.e. efficiency.

#### Temperature programming plays an important role.

Either linearly or in different ramps and gradients - the order of elution of analytes (according to the significance of influences – b.p.t., affinity) and resolution can also be influenced.

#### SEPARATION OF MEMBERS OF HOMOLOGOUS SERIES

Temperature changes have a similar effect on retention of all analytes

#### SEPARATION OF COMPOUNDS OF DIFFERENT CHARACTER

Temperature changes have a major effect on the separation

A minimal change in temperature may have a more significant effect on the separation than a change of SP film thickness or column length

### Inert, no influence on sorption – desorption, selectivity

- type and velocity affect efficiency and analysis time

### Linear velocity - u (cm/s)

- velocity of carrier gas moving through column
- dissimilar across a column average value is used

#### Van Deemter curve

- relation of **u** and efficiency expressed as **h** (HETP)
- $h_{min} \approx$  the most theoretical levels, i.e. the highest efficiency

$$\mathbf{h} = \mathbf{A} + \mathbf{B} / \mathbf{u} + \mathbf{C} \mathbf{u}$$

Golay's equation for capillary columns - does not contain A (sorbent)

$$h = B/u + Cu$$

- ↓ u = low analyte velocity in column = more mass transfers MP ⇔ SP
   ⇒ large longitudinal diffusion (zones overlap)
- ↑ u = minimal longitudinal diffusion

  ⇒ only a limited number of mass transfers

#### **OPTIMAL LINEAR VELOCITY**

it is therefore a compromise for these opposing phenomena.

### **Highest efficiency (h<sub>min</sub>)**

Optimal value of **u** - low (small flows) and very narrow range

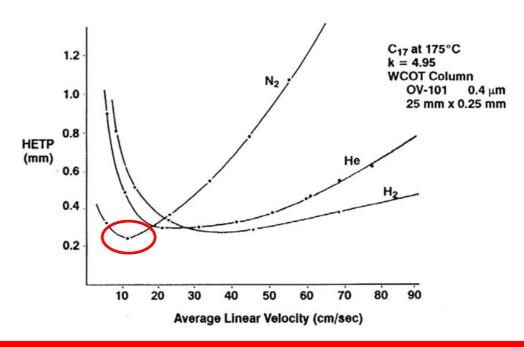
 $\Rightarrow$  high retention times

Curve is very steep  $\Rightarrow$  small increase in velocity

 $\Rightarrow$  big change in efficiency

When programming temperature, constant flow is recommended.

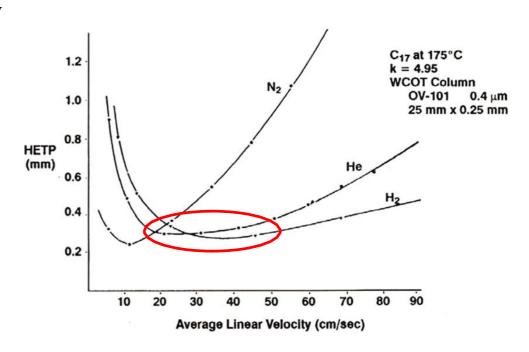
- cheap and affordable
- possibility of production using generator



### Acceptably high efficiency $(h_{min})$ - lower than for $N_2$

Optimal value of **u** - high enough and larger range

- ⇒ lower retention times the curve is not so steep
- $\Rightarrow$  velocity increase = small change in efficiency
- expensive and limitedly available
- price increases



### High efficiency $(h_{min})$ – between $N_2$ and He

Optimal value of **u** - high and large range

- ⇒ lower retention times the curve is flat
- ⇒ velocity increase = minimum change in efficiency
- reasonable price and availability
- possibility of production using generator
- risk of explosion

